

FORM PTO-1390
(REV. 5-93)U.S. DEPARTMENT OF COMMERCE
PATENT AND TRADEMARK OFFICEATTORNEY'S DOCKET NUMBER
2345/170TRANSMITTAL LETTER TO THE UNITED STATES
DESIGNATED/ELECTED OFFICE (DO/EO/US)
CONCERNING A FILING UNDER 35 U.S.C. 371

U.S. APPLICATION NO. (If known, see 37 CFR 1.5)

09/980250

INTERNATIONAL APPLICATION NO.
PCT/EP00/04167INTERNATIONAL FILING DATE
10 May 2000
(10.05.00)PRIORITY DATE CLAIMED:
25 May 1999
(25.05.99)TITLE
MINIATURIZED TERAHERTZ RADIATION SOURCEAPPLICANT(S) FOR DO/EO/US
Hans W. P. KOOPS; Tobias BAUER; Wolfgang Elsaesser; Filip FLOREANI; and Hartmut ROSKOS

Applicant(s) herewith submits to the United States Designated/Elected Office (DO/EO/US) the following items and other information

1. This is a **FIRST** submission of items concerning a filing under 35 U.S.C. 371.
2. This is a **SECOND** or **SUBSEQUENT** submission of items concerning a filing under 35 U.S.C. 371.
3. This is an express request to begin national examination procedures (35 U.S.C. 371(f)) immediately rather than delay examination until the expiration of the applicable time limit set in 35 U.S.C. 371(b) and PCT Articles 22 and 39(1).
4. A proper Demand for International Preliminary Examination was made by the 19th month from the earliest claimed priority date.
5. A copy of the International Application as filed (35 U.S.C. 371(c)(2))
 - a. is transmitted herewith (required only if not transmitted by the International Bureau).
 - b. has been transmitted by the International Bureau.
 - c. is not required, as the application was filed in the United States Receiving Office (RO/US)
6. A translation of the International Application into English (35 U.S.C. 371(c)(2)).
7. Amendments to the claims of the International Application under PCT Article 19 (35 U.S.C. 371(c)(3))
 - a. are transmitted herewith (required only if not transmitted by the International Bureau).
 - b. have been transmitted by the International Bureau.
 - c. have not been made; however, the time limit for making such amendments has NOT expired.
 - d. have not been made and will not be made.
8. A translation of the amendments to the claims under PCT Article 19 (35 U.S.C. 371(c)(3)).
9. An oath or declaration of the inventor(s) (35 U.S.C. 371(c)(4)). (UNSIGNED)
10. A translation of the annexes to the International Preliminary Examination Report under PCT Article 36 (35 U.S.C. 371(c)(5)).

Items 11. to 16. below concern other document(s) or information included:

11. An Information Disclosure Statement under 37 CFR 1.97 and 1.98.
12. An assignment document for recording. A separate cover sheet in compliance with 37 CFR 3.28 and 3.31 is included.
13. A **FIRST** preliminary amendment.
- A **SECOND** or **SUBSEQUENT** preliminary amendment.
14. A substitute specification and a marked up version of the substitute specification.
15. A change of power of attorney and/or address letter.
16. Other items or information: International Search Report and Form PCT/RO/101.

Express Mail No.: EL179952330US

17. The following fees are submitted:

Basic National Fee (37 CFR 1.492(a)(1)-(5)):

Search Report has been prepared by the EPO or JPO \$890.00

International preliminary examination fee paid to USPTO (37 CFR 1.482) \$710.00

No international preliminary examination fee paid to USPTO (37 CFR 1.482) but
international search fee paid to USPTO (37 CFR 1.445(a)(2)) \$740.00Neither international preliminary examination fee (37 CFR 1.482) nor international
search fee (37 CFR 1.445(a)(2)) paid to USPTO \$1,040.00International preliminary examination fee paid to USPTO (37 CFR 1.482) and all
claims satisfied provisions of PCT Article 33(2)-(4) \$100.00

CALCULATIONS | PTO USE ONLY

ENTER APPROPRIATE BASIC FEE AMOUNT = \$890

Surcharge of \$130.00 for furnishing the oath or declaration later than 20 30 months
from the earliest claimed priority date (37 CFR 1.492(e)).

Claims	Number Filed	Number Extra	Rate	
Total Claims	23 - 20 =	3	X \$18.00	\$54
Independent Claims	1 - 3 =	0	X \$84.00	\$0
Multiple dependent claim(s) (if applicable)			+ \$280.00	\$

TOTAL OF ABOVE CALCULATIONS = \$944

Reduction by 1/2 for filing by small entity, if applicable. Verified Small Entity statement must
also be filed. (Note 37 CFR 1.9, 1.27, 1.28).

SUBTOTAL = \$944

Processing fee of \$130.00 for furnishing the English translation later the 20 30
months from the earliest claimed priority date (37 CFR 1.492(f)).

TOTAL NATIONAL FEE = \$944

Fee for recording the enclosed assignment (37 CFR 1.21(h)). The assignment must be
accompanied by an appropriate cover sheet (37 CFR 3.28, 3.31). \$40.00 per property+ \$ Amount to be
refunded
charged \$

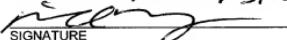
TOTAL FEES ENCLOSED = \$944

a. A check in the amount of \$ _____ to cover the above fees is enclosed.

b. Please charge my Deposit Account No. 11-0600 in the amount of \$944.00 to cover the above fees. A duplicate copy of this sheet is enclosed.

c. The Commissioner is hereby authorized to charge any additional fees which may be required, or credit any overpayment to Deposit Account No. 11-0600. A duplicate copy of this sheet is enclosed.

NOTE: Where an appropriate time limit under 37 CFR 1.494 or 1.495 has not been met, a petition to revive (37 CFR 1.137(a) or (b)) must be filed and granted to restore the application to pending status.


SIGNATURE

Richard L. Mayer, Reg. No. 22,490

NAME

11/26/01

DATE

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[2345/170]

IN THE UNITED STATES PATENT AND TRADEMARK OFFICE

Applicant(s) : Hans W. P. KOOPS et al.
Serial No. : To Be Assigned
Filed : Herewith
For : MINIATURIZED TERAHERTZ RADIATION SOURCE
Art Unit : To Be Assigned
Examiner : To Be Assigned

Assistant Commissioner
for Patents
Washington, D.C. 20231

PRELIMINARY AMENDMENT AND
37 C.F.R. § 1.125 SUBSTITUTE SPECIFICATION STATEMENT

SIR:

Please amend without prejudice the above-identified application before examination, as set forth below.

IN THE TITLE:

Please replace the title with the following:
--MINIATURIZED TERAHERTZ RADIATION SOURCE--.

IN THE SPECIFICATION AND ABSTRACT:

In accordance with 37 C.F.R. § 1.121(b)(3), a Substitute Specification (including the Abstract, but without claims) accompanies this response. It is respectfully requested that the Substitute Specification (including Abstract) be entered to replace the Specification of record.

A demand for International Preliminary Examination was made on November 2, 2000.

IN THE CLAIMS:

Without prejudice, please cancel original claims 1 to 23 in the original application and and please add new claims 24 to 46 as follows:

NY01 398577 v 1 8L179952330

24. (New) A miniaturized terahertz radiation source based on the Smith-Purcell effect, comprising:

- a field emitter;
- an electrostatic lens;
- a beam deflector;
- a grating of metal; and
- a second anode;

wherein the field emitter, the electrostatic lens, the beam deflector, the grating of metal and the second anode are integrated on a semiconductor chip using one of additive and nanolithographic methods,

and wherein from a focused electron source, a high-energy bundle of electrons is transmitted at a defined distance over a reflection diffraction grating having transversely disposed grating rods so that in response to an image charge oscillating within a profile of the reflection diffraction grating an electromagnetic wave of a wavelength is emitted and is adjustable as a function of a periodicity of lines and of electron velocity.

25. (New) The miniaturized terahertz radiation source of claim 24, wherein the electron source is a wire constructed using additive nanolithography out of readily conductive material having stabilizing series resistance,

and wherein the wire is positioned using computer-controlled deposition lithography in at least one of a straight design and a curved design to end freely over a surface of a conductor path structure for any electrical terminals and connections in any tips of the field emitter.

26. (New) The miniaturized terahertz radiation source of claim 24, wherein the electron source has a punctiform design and a material, having a low work function and emits electrons at least in response to relatively low voltages, and is deposited on any tips of the field emitter using additive nanolithography.

27. (New) The miniaturized terahertz radiation source of claim 24, wherein the field emitter, the electrostatic lens, the beam deflector, the grating of metal, and the second anode, are encapsulated in a vacuum-tight manner by a covering chip.

28. (New) The miniaturized terahertz radiation source of claim 24, wherein the beam deflector is configured to deflect an electron beam in a horizontal direction and a vertical direction, the grating of metal is configured to have an underlaid reflector constructed in integrated fashion, using mix-match technology, employing one of additive nanolithography, electron beam lithography, and optical lithography, on prefabricated metal conductor connection structures having integrated grating structures, on a layer of silicon dioxide of a substrate of silicon, having a THz reflector base in a grating region, all being an imperviously encapsulated structure so as to be transparent to terahertz radiation, and

the electron beam emerging from the electron source is configured to be focused through an electrostatic lens in the form of miniaturized wire lenses and is configured to be guided and positioned by integrated deflecting plates in relation to a position of the reflection diffraction grating, and

a terahertz radiation is configured to be producable to have an intensity and wavelength which are variable and selectable.

29. (New) The miniaturized terahertz radiation source of claim 24, wherein to accelerate the electrons behind the electron source, an accelerator grid in form of a free-standing electrode having at least one of two cylindrical rods and a standing wire ring is positioned behind the field electron source; and

any accelerated electrons arrive in one of round multipole lenses and cylindrical lenses of an electrostatic lens configured subsequent to the accelerator grid, and the electron beam propagates without being deflected over a subsequent reflection diffraction grating at a homogeneous distance to a surface.

30. (New) The miniaturized terahertz radiation source of claim 24, wherein the reflection diffraction grating, having a length of approximately 1 mm to 1 cm and grating periods of approximately 0.5 to 10 μ m, depending on a wavelength of a terahertz radiation to be emitted, is positioned subsequent to the electrostatic lens and the beam deflector which are implemented using additive nanolithography on a metal structure produced using one of electron-beam lithography and optical lithography.

31. (New) The miniaturized terahertz radiation source of claim 24, further comprising:

a plurality of electrically isolated diffraction gratings positioned side-by-side in a gratings of metal manner, the plurality of electrically isolated diffraction gratings being configured to be activated in response to selection of various sources for selecting different emitted wavelengths.

32. (New) The miniaturized terahertz radiation source of claim 28, further comprising ionic getter materials, capable of being activated by an electrode, applied to the semiconductor chip near to a Smith-Purcell element, to produce and maintain a required vacuum in the encapsulated structure.

33. (New) The miniaturized terahertz radiation source of claim 25, further comprising a controllable voltage source connected via at least one of an electrical terminals and connections to the electron source to stabilize radiation from the electron source;

and wherein the electron beam exiting any tips of the field emitter is collected on an electrode of the second anode.

34. (New) The miniaturized terahertz radiation source of claim 24, wherein to precisely adjust the wavelength and/or generate a desired frequency spectrum, a voltage is applied between an earth electrode of the electrostatic lens and an electrode acting as the second anode to alter the electron velocity along a grating.

35. (New) The miniaturized terahertz radiation source of claim 24, wherein the miniaturized terahertz radiation source is covered by a membrane window etched using a silicon membrane technique and is configured to be evacuated in a vacuum system prior to a bonding operation to a pressure within a range of 10^{-4} Torr, which suffices for an average free path length of one millimeter; and

further comprising at least one chamber constructed in the vacuum system using thermal bonding so as to be able to be at least one of encapsulated and sealed without short-circuiting a voltage supply.

36. (New) The miniaturized terahertz radiation source of claim 24, wherein two membrane windows are positioned next to one another in a covering chip for two chambers; and

in one of the two membrane windows a getter pump is set in operation by a one-time activation in response to current flow, and the entire volume of the two chambers receives a required operating pressure.

37. (New) The miniaturized terahertz radiation source of claim 36, wherein the two membrane windows in the covering chip are treated with additionally applied layers to reduce reflection.

38. (New) The miniaturized terahertz radiation source of claim 24, further comprising a terahertz radiation reflector configured underneath a grating region, the terahertz radiation reflector being configured as one of a metal layer and an arrangement of grating rods, and having a defined spacing of a suitable period, having at least one of a magnetic and non-magnetic material to strengthen an intensity of emitted terahertz radiation.

39. (New) The miniaturized terahertz radiation source of claim 38, wherein an intensity of the radiation source is variable in response to beam guidance over the grating of metal at a defined distance; the radiated intensity is configured to be modulated in response to an application of an alternating current voltage to a deflecting element, by employing an additional deflecting element before the grating of metal.

40. (New) The miniaturized terahertz radiation source of claim 24, wherein the radiation source is configured to generate terahertz radiation as modulated radiation for spectroscopic purposes, and wherein the modulated radiation is generatable by modulating an extraction voltage at any tips of the field emitter.

41. (New) The miniaturized terahertz radiation source of claim 24, further comprising a monochromator on an overlying surface in form of one of a nanometer structure and a micrometer structure that acts on a region; and wherein terahertz radiation is configured generatable with a different wavelength and exits the radiation source in different directions.

42. (New) The miniaturized terahertz radiation source of claim 24, wherein an electrical field is applied between the electrostatic lens for focusing and an end of the grating of metal,

an additional electrode of the second anode is positioned at the end of the grating of metal which, through an applied voltage, either accelerates or decelerates flying electrons.

43. (New) The miniaturized terahertz radiation source of claim 24, wherein the grating of metal is subdivided into regions which are disposed in parallel to a beam direction and in which different grating constants are implemented, and wherein a lateral deflecting element for at least one of beam guidance and wavelength selection is mounted around grating regions, and/or groups of field emitters are selectively driven.

44. (New) The miniaturized terahertz radiation source of claim 24, wherein the grating of metal varies in its grating constant transversely to the beam direction so that deflection fields or deflecting plates, which surround the grating of metal all around, are positioned as beam deflectors, such that a beam guidance over the grating of metal is variable in such a way that one region having a different grating constant is selected for emitting a wavelength of terahertz radiation and if the grating of metal has a variable grating constant then the wavelength of the terahertz radiation is continuously adjustable.

45. (New) The miniaturized terahertz radiation source of claim 24, wherein an electrostatic plate is transparent to the terahertz radiation and is positioned to provide intensity control below and above the grating of metal, and enables a position of the electron beam to be varied in an entire grating region.

46. (New) The miniaturized terahertz radiation source of claim 24, wherein the radiation source is designed as a component that is available in modular form and is usable in any spatial situation.

REMARKS

This Preliminary Amendment cancels without prejudice original claims 1 to 23 in the underlying PCT Application No. PCT/EP00/04167, and adds without prejudice new claims 24 to 46. The new claims conform the claims to U.S. Patent and Trademark Office rules and do not add new matter to the application.

In accordance with 37 C.F.R. § 1.121(b)(3), the Substitute Specification (including the Abstract, but without the claims) contains no new matter. The amendments reflected in the

Substitute Specification (including Abstract) are to conform the Specification and Abstract to U.S. Patent and Trademark Office rules or to correct informalities. As required by 37 C.F.R. § 1.121(b)(3)(iii) and § 1.125(b)(2), a Marked Up Version Of The Substitute Specification comparing the Specification of record and the Substitute Specification also accompanies this Preliminary Amendment. In the Marked Up Version, double-underlining indicates added text and bracketing indicates deleted text. Approval and entry of the Substitute Specification (including Abstract) is respectfully requested.

The underlying PCT Application No. PCT/EP00/04167 includes an International Search Report, dated November 16, 2000. The Search Report includes a list of documents that were uncovered in the underlying PCT Application. A copy of the Search Report accompanies this Preliminary Amendment.

Applicants assert that the subject matter of the present application is new, non-obvious, and useful. Prompt consideration and allowance of the application are respectfully requested.

Respectfully Submitted,

KENYON & KENYON

By: 

By: 

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MINIATURIZED TERAHERTZ RADIATION SOURCE

FIELD OF THE INVENTION

The present invention relates to a miniaturized terahertz radiation source that is based on the Smith Purcell effect.

BACKGROUND INFORMATION

At certain frequencies in the far infrared range, coherent radiation may be generated, for example, by molecular lasers which are pumped by CO_2 lasers. Many of the frequencies and wavelengths of importance to the spectroscopy of molecules and solid bodies may be within the wavelength range extending from 3 mm to 30 μm (from 100 gigahertz to 10 terahertz). The use of a microradiation source, which may be tunable within the wavelength range and implemented on a semiconductor chip of a wafer for this range of terahertz radiation and which exhibits sufficient power output within the range of between 1 μW and 1 W, may be substantially significant from a technical standpoint for spectroscopic applications in all areas of environmental protection, analytics, and in material characterization in medicine and biology, as well as in chemistry and physics. Another way to generate coherent radiation in the far infrared range is based on the so-called Smith Purcell effect. It provides for generating radiation similar to the method known from the "free electron laser". Macroscopic electron sources and diffraction gratings having a 100 to 300 μm period may be used to generate a coherent radiation field of polarized radiation having up to 1 μW power.

The reference "Intensity of Smith-Purcell Radiation in the Relativistic Regime", J. Walsh, K. Woods, S. Yeager, Department of Physics and Astronomy, Dartmouth College,

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Hanover, N.H. 03755, U.S., pages 277-279, discusses the theory of such Smith-Purcell radiation sources and, additionally, gives experimental results. The reference "A New Source of THz-FIR Radiation" in LEOS NEWSLETTER, February, 1999 by J.E. 5 Walsh, J.H. Brownell, J.C. Swartz, Department of Physics and Astronomy, Dartmouth College, Hanover, New Hampshire 03755-3528 and M.F. Kimmitt, Department of Physics, Essex University, Colchester, UK, January 7, 1999, pages 11-14, discusses the design and mode of operation of a radiation 10 source in the terahertz region. It may be that these terahertz radiation sources are perfectly efficient, but they do not yet suffice for many analytical applications, and they are not yet miniaturized to a sufficient degree.

15 **SUMMARY OF THE INVENTION**

The present invention is directed to providing a free electron laser, which is miniaturized further extent, and may be a more powerful source for analytical applications.

20 Exemplary embodiments and/or exemplary methods of the present invention are directed to providing a miniaturized terahertz radiation source, which is based on the Smith-Purcell effect, on a semiconductor chip, using available additive nanolithography, which may function as a miniaturized, free 25 electron laser, be substantially more powerful than existing such radiation sources, and facilitate a substantially broader field of application, in particular for analytical applications.

30 Exemplary embodiments and/or exemplary methods of the present invention are further directed to using additive nanolithography to produce such miniaturized terahertz radiation sources, such that field electron sources having a high directional beam value may be produced. By employing 35 additional miniaturized, electron-optical elements, for example, accelerator grids, focusing lenses, beam deflectors,

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and free-standing metallic rods, the components may now be assembled to construct a miniaturized, free electron laser on a surface of a few $100 \mu\text{m}^2$ through 10 mm^2 . In this context, the electron source has the characteristic of emitting electrons 5 at 30 volts, which then possess an energy of 30 electron volts. In exemplary embodiments and/or exemplary methods of the present invention, using nanolithography, the second characteristic component of focusing and beam guidance of the electron beam in parallel to the surface at a finite distance 10 to the third component, a metallic grating, may be controlled. The vertical position or height of the beam over the metallic grating may likewise be adjusted by applying deflection 15 voltages to micro-miniaturized deflecting plates or wire lenses. The diffraction grating, to the extent that is possible, up to one millimeter long, a reflection diffraction 20 grating having a grating constant in the range of 0.1 mm to 0.1 μm , may be produced using conventional lithography in the manufacturing of electrical connection structures for supplying the field electron source, i.e., be defined by 25 electron-beam lithography at the highest resolutions.

In exemplary embodiments and/or exemplary methods of the present invention, a high-resolution double-resist technique and lift-off may be used. The exemplary embodiments and/or 25 exemplary methods may employ new types of technologies to integrate the electron source, the beam guidance, and the generation of the far-infrared radiation by the flight of the fast electrons across the diffraction grating. In this context, given standard sources of up to approximately 20,000 30 volts accelerating voltage and an electron beam of $20 \mu\text{m}$ diameter over a grating of 100 to $300 \mu\text{m}$ period, an infrared radiation in the far infrared is achieved between $100 \mu\text{m}$ and one millimeter wavelength. This radiation may be produced by the image charge, or image potential energy, which oscillates 35 in response to the electrons flying past the surface profile of the grating. The changing spacing between the charges

produces an oscillating dipole, which may oscillate in
coherent fashion along the grating. This ensues due to the
Coulomb interaction of the individual charges on the wires. In
this context, the entire electrical field may oscillate
5 coherently in conformance with the individual charges of the
rods. In this manner, electromagnetic radiation is emitted
coherently along the entire grating. Its energy transfer from
the electron beam to the electromagnetic radiation takes place
virtually losslessly. The polarization may require a certain
10 displacement current and, thus, a certain power, but this may
be entirely drawn directly from the beam. In exemplary
embodiments and/or exemplary methods of the present invention,
the oscillating dipole charge chain may be produced in this
manner. In further exemplary embodiments and/or exemplary
15 methods of the present invention, integration of the electron
guidance on a chip, and the direct coupling to the grating
having a high spatial resolution, in the manufacturing process
is provided. In further exemplary embodiments and/or
exemplary methods of the present invention,
20 micro-miniaturization may allow for the use of low-energy
electrons having energies of between 10 and 1000 eV. Further
exemplary embodiments and/or exemplary methods are directed to
generating up to 10 kV of electrons on the chip and to
implement the guidance by using miniaturized electron-optical
25 components, such as micro-lenses and deflecting elements.

In further exemplary embodiments and/or exemplary methods of
the present invention, when using such high-energy electrons,
radiation may also be generated for short wavelengths ranging
30 from middle infrared to the visible spectral region. By
manufacturing on a common substrate, one ensures direct
coupling to the grating via the shortest distance to the
source, and the manufacturing of the grating and the source on
the same chip. In this manner, in further exemplary
35 embodiments and/or exemplary methods, the path of rays of the
electrode configuration, which in a conventional design, may

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be up to one meter, is reduced to less than 1 mm to 10 mm
length. Moreover, a very highly coherent and local light
source may be produced, which benefits the temporal and spatial
coherence of the radiation. In exemplary embodiments and/or
5 exemplary methods of the present invention, because the entire
electron path is shortened to a greater degree, it may be no
longer necessary to use extra-high or high vacuum in the
radiation room. It may suffice to cover the system by a window
etched in silicon using a flipchip bonding technique. This
10 window may be closed by a continuous membrane of silicon,
thereby rendering possible a hollow space. The up to 10 μm
high component may be easily accommodated in the hollow space.
15 Into a silicon wafer of 250 μm thickness, one may etch windows
of a few millimeter diameter, which are sealed by a membrane
having a thickness of 10 μm up to 100 μm . This may render a
stable mechanical encapsulation of the miniaturized component.
20 In exemplary embodiments and/or exemplary methods of the
present invention, it can also be manufactured
micromechanically, in millimeter dimensions. In this context,
the required vacuum is approximately 0.01 Torr. In this case,
25 the average free path length of the electrons in this gas of
reduced pressure is as large as the beam length of the
miniaturized component. This can eliminate the need for a pump
configuration. The component can be packaged as a ready-made,
sealed element and connected. In this manner, a terahertz
30 radiation source may be produced, i.e., a millimeter and
submillimeter radiation source on a semiconductor chip.
Through appropriate wave guidance, this radiation source can
be linked to further applications.

30 BRIEF DESCRIPTION OF THE DRAWINGS

Figure 1 shows a plan and side view of a fundamental design of
a miniaturized terahertz radiation source based on the Smith
Purcell effect.

35 Figure 2 shows an encapsulation having a silicon membrane

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structure for maintaining the necessary vacuum during
operation.

Figure 3 shows a two-chamber membrane covering of the
5 miniaturized, free electron laser.

DETAILED DESCRIPTION

Figure 1 schematically depicts the electrode design for a
miniaturized, free electron laser in a plan view and side
10 view. The individually illustrated elements may also be
produced using an available additive nanolithography method.
Shown both in the plan view as well as in the side view, the
individual elements of the miniaturized terahertz radiation
source are illustrated in the following sequence. First, field
15 emitter tips 1 are shown to the left. They are linked via
electrical terminals or connections 2 to a controllable
voltage source 3 and, on the other hand, to an electrostatic
lens 4, composed here of three electrodes. The left electrode
is the extractor or the first anode of the electron source.
20 Shown in the middle are beam deflectors 5 having connections
6, to which optical and/or electron-beam lithography and a
deflection voltage are applied. Beam deflector 5 is followed
by a grating 7 of metal. Electron beam 9, having been
deflected by beam deflector 5, passes through this grating and
25 strikes here as an electron beam, without being deflected 10,
upon a second anode 8.

Figure 2 shows an exemplary variant of an encapsulation. This
design enables the electron source, here in the form of field
30 emitter tips 1, electrostatic lens 4 for focusing electron
beam 9/10, beam deflector 5 for deflecting the beam in the
horizontal and vertical direction, grating 7 of metal having
an underlaid reflector to be constructed in integrated
fashion, using mix-match technology employing additive
35 nanolithography on an insulating substrate having a terahertz
reflection base in the grating region, on metal conductor

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connection structures, which are prefabricated using electron beam or optical lithography, and to be imperviously encapsulated in a vacuum 13 using a technology which is transparent to terahertz radiation. This design enables

5 electron beam 9 emerging from field emitter 1 to be focused through miniaturized wire lenses 4, to be directed through integrated deflecting plates 5 relatively to the position of grating 7, and to be positioned, thereby generating terahertz radiation, whose intensity and wavelength may be varied and

10 selected. Field emitters, i.e., field emitter tips 1 are linked via an electrical terminal connection 2 to a controllable voltage source 3 and, moreover, via an electrical connection 2 to the middle electrode of electrostatic lens 4. The left electrical electrode of lens 4 is the first anode of

15 the electron source and, together with a terminal of controllable voltage source 3, is connected to ground, as is also the electrode of electrostatic lens 4 situated on the other side of the middle electrode. The field electron source having field emitters 1 is a wire constructed, using additive nanolithography, out of readily conductive material having stabilizing series resistance, and may be designed such that electron beam 9 emerges in parallel to the surface. This means that the wire is manufactured, using a computer-controlled deposition lithography, in a straight or curved design, to end

20 freely over the surface of the conductor path structure. The field electron source has a punctiform design. On its field emitter tips (1), a material having a low work function is deposited using additive nanolithography, so that electrons are emitted already in response to relatively low voltages.

25

30 An exemplary variant of the design provides for mounting an accelerator grid as a beam deflector 5, in the form of a free-standing electrode composed of two cylindrical rods or a standing wire ring, behind the field electron source having

35 field emitters 1. The electrons may thus be accelerated and directed into subsequent, additionally constructed round

5 multipole lenses and/or cylindrical lenses, so that the
propagating electron beam 9 is additionally deflected over
subsequent diffraction grating 7 at a homogeneous distance to
the surface. The focusing and beam-guidance lenses, which are
10 implemented by additive nanolithography on the metal
connection structure produced using electron-beam lithography
or optical lithography, are constructed, using this
technology, to produce a diffraction grating having a length
of approximately 1 mm to 1 cm, with grating periods of 0.5 to
15 μm , depending on the wavelength of the terahertz radiation
to be emitted.

20 An exemplary variant of the design may also provide for a
side-by-side configuration of a plurality of electrically
15 isolated diffraction gratings, which may be activated by
selecting various sources, enabling various emitted
wavelengths to be chosen.

25 The radiation from electron source is retained at a constant
level by a control circuit, in particular by a controllable
voltage source 3, and electron beam 10 propagating over
20 grating 7 is then picked up by a second anode 8, which is used
as a collecting anode electrode.

30 Between the second earth electrode of electrostatic lens 4 and
second anode 8, a field is applied, which may be used to alter
the electron velocity along the grating. This may be used for
precisely adjusting the wavelength and also for generating a
frequency spectrum.

35 Another exemplary embodiment of the design of the
miniaturized, i.e., microminiaturized terahertz radiation
source, based on the Smith-Purcell effect, is shown in Figure
2. By providing encapsulation using a silicon membrane
35 structure, the required vacuum 13 may be maintained for
operating the laser. The emitted laser THz radiation 15 is

radiated to the outside through a membrane window 14. The
radiation emitter, constructed on a chip of silicon 11 and
composed of the field emission source, optics, grating and
anode, is covered in this exemplary embodiment by membrane
5 window 14, which is made of silicon 11, as may be the entire
covering chip 16. The thus constructed radiation emitter may
be evacuated in a vacuum system, prior to the bonding, to a
pressure of 10^{-4} , which suffices for one millimeter average
free path length. The hollow space may subsequently be sealed
10 in the vacuum by thermal bonding, without short-circuiting the
voltage supply. Membrane windows 14 in covering chip 17 may be
treated using reflection-reducing layers, so that a maximum
transmission through window 14 is attained for the frequency
range of the emitted radiation.

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Further, configured underneath the grating region may be a THz
radiation reflector in the form of a metal layer or
arrangement of grating rods, having a defined spacing of a
suitable period, of magnetic or non-magnetic materials, so THz
radiation 15, which exits grating 7 in the direction of the
substrate, may be sent back through the grating with the
highest possible reflectance, thereby strengthening the
intensity of the emitted radiation. Implementing a beam
guidance over grating 7 at a defined distance can may allow
variation of the intensity of the radiation source. This means
that by employing deflecting element 5 before the grating, the
radiated intensity may be modulated in response to the
application of an alternating current voltage to this
deflecting element. In this manner, the radiation may be
directly generated in modulated form for spectroscopic
purposes for lock-in measuring techniques. The same lock-in
modulation may also be provided by modulating the extraction
voltage at field emitter tip 1.

35 For certain applications, the voltage source may be
supplemented by installing a monochromator on an overlying

surface. Such a monochromator may be constituted as a nanometer structure or micrometer structure that acts on this region, so that beams generated with a different wavelength exit the radiation source in different directions. In this 5 manner, by switching over the electron energy, which, in the electrostatic system in accordance with the electrostatic principle, may always yield the same focusing and, thus, constant operating conditions, radiation of different frequencies may be generated, and the radiation source may be 10 electrically tuned for different applications.

Between focusing lens 4 and the end of grating 7, one variant provides for applying an electrical field, in which, at the end of the grating, an additional electrode is positioned, 15 through which voltage may be applied to accelerate or decelerate the flying electrons. This makes it possible to compensate for the energy loss experienced by the electrons when flying past grating 7. Grating 7, over which electron beam 10 propagates, may be subdivided into regions which are 20 disposed in parallel to the beam direction, in which different grating constants are implemented. The horizontal, electrostatic beam guidance, effected by electrodes positioned in parallel to grating 7 and, respectively, by a plurality of electron sources, one of which is assigned to the individual 25 region, may allow for the emitted radiation to be implemented as radiation that is switchable in its wavelength.

The grating constant of the grating may vary transversely to the beam direction, so that the beam guidance may be varied 30 over the grating by deflection fields or by deflecting plates, which surround the grating all around, and are positioned behind the focusing lens, such that a region having a different grating constant may be selected for emitting the wavelength of the radiation. Designing the grating as a 35 "chirped grating", i.e., as a grating having a variable grating constant, enables the wavelength to be adjusted in

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continuous fashion.

The intensity of the terahertz radiation source is controlled by installing an electrostatic plate, which is transparent to THz radiation, below and above the grating, thereby enabling the intensity to be locally selected, or selected with respect to particular locations. This may be achieved by designing these electrostatic plates to include regions of different potentials, i.e., by providing separately adjustable strips.

Figure 3 shows another exemplary embodiment, where two membrane windows 14 are provided in covering chip 17. As in Figure 2, covering chip 17 may be insulated from the electrodes and the electrode connections by an insulator of silicon 16. At the same time, this is also constituted of bond region 7 for providing hermetic sealing when encapsulating the arrangement. The construction includes, in turn, the substrate of silicon 11 having a silicon dioxide layer 12. Positioned thereon are field emitter 1, lenses 4, grating 7 and second anode 8. The first anode is the left electrode of electrostatic lens 4. Also positioned, in turn, is grating 7 of metal, out of which the emitted terahertz radiation 15 emerges. Electron beam 10 impinges, without deflection, on second anode 8 having electrical connection 2. The one membrane window 14 is provided with a lens 19 for focusing THz radiation 15. Due to the specially formed covering chip 17, a vacuum 13 may be provided in both chambers 18, 18'; a getter pump, including its material, may be set in operation in second chamber 18' by a one-time activation in response to current flow, to bring the entire volume of both chambers to the required operating pressure.

In a further exemplary variant, ionic getter materials, capable of being activated by the electrical connection, are applied to the chip, next to the Smith-Purcell element. These materials may be used for pumping out the bonded and

encapsulated structure. Such a manufacturing, employing additive nanolithography on metal conductor-connection structures, which are prefabricated by electron beam lithography or optical lithography, may include integrated grating structures on an insulating substrate, such as silicon oxide, and a THz underlaid reflector integrated in the grating region, renders possible a component which may be used and set up in any position as a THz radiation source in modular form.

10 G. G. BURGESS

ABSTRACT OF THE DISCLOSURE

A miniaturized terahertz radiation source based on the Smith-Purcell effect is provided, in which, from a focused 5 electron source, a high-energy bundle or beam of electrons is transmitted at a defined distance over a reflection diffraction grating composed of transversely disposed grating rods, so that, in response to oscillating image charges, electromagnetic waves of one wavelength are emitted, the 10 wavelength being adjustable as a function of the periodicity of the lines and of the electron velocity. The elements of the radiation source, such as field emitter, electrostatic lens, beam deflector, grating of metal, and a second anode, are integrated on a semiconductor chip using additive 15 nanolithographic methods. The field electron source is constructed to project, as a wire, out of the surface, using additive nanolithography, and is made of readily conductive material having stabilizing series resistance. The wire is constructed, using computer-controlled deposition lithography, 20 in a straight or curved, free-standing design. In its surface area, the base material bears a conductor structure for the electrical terminals and connections, including controllable voltage sources for supplying the field emitter tips, lens, and control electrodes. The terahertz radiation source is 25 designed to be a powerful component that may be available in modular form and may be usable in any spatial situation.

MINIATURIZED TERAHERTZ RADIATION SOURCE

The present invention is directed to a miniaturized terahertz radiation source that is based on the Smith Purcell effect according to the definition of the species in Claim 1.

It is fundamentally known that, at certain frequencies in the far infrared range, coherent radiation can be generated, for example, by molecular lasers which are pumped by CO_2 lasers. Many of the frequencies and wavelengths of importance to the spectroscopy of molecules and solid bodies are within the wavelength range extending from 3 mm to 30 μm (from 100 gigahertz to 10 terahertz). The use of a microradiation source, which is tunable within the wavelength range and is implemented on a semiconductor chip of a wafer, for this range of terahertz radiation, which exhibits sufficient power output within the range of between 1 μW and 1 W, is substantially significant from a technical standpoint for spectroscopic applications in all areas of environmental protection, analytics, and in material characterization in medicine and biology, as well as in chemistry and physics. Another way to generate coherent radiation in the far infrared range is based on the so-called Smith Purcell effect. It provides for generating radiation similarly to the method known from the "free electron laser". Macroscopic electron sources and diffraction gratings having a 100 to 300 μm period are used to generate a coherent radiation field of polarized radiation having up to 1 μW power.

The article "Intensity of Smith-Purcell Radiation in the Relativistic Regime", J. Walsh, K. Woods, S. Yeager, Department of Physics and Astronomy, Dartmouth College, Hanover, N.H. 03755, U.S., pages 277-279, discusses the theory

of such Smith-Purcell radiation sources and, additionally, gives experimental results. Also, the article entitled "A New Source of THz-FIR Radiation" in LEOS NEWSLETTER, February, 1999 by J.E. Walsh, J.H. Brownell, J.C. Swartz, Department of Physics and Astronomy, Dartmouth College, Hanover, New Hampshire 03755-3528 and M.F. Kimmitt, Department of Physics, Essex University, Colchester, UK, January 7, 1999, pages 11-14, fundamentally describes the design and mode of operation of a radiation source in the terahertz region. It may be that these known terahertz radiation sources are perfectly efficient, but they do not yet suffice for many analytical applications, and they are not yet miniaturized to a sufficient degree.

For that reason, a free electron laser, which is miniaturized further extent, is desired as a more powerful source for analytical applications.

The underlying object of the present invention is, therefore, to devise a miniaturized terahertz radiation source, which is based on the Smith-Purcell effect, on a semiconductor chip, using the known additive nanolithography, which will function as a miniaturized, free electron laser, be substantially more powerful than existing such radiation sources, and facilitate a substantially broader field of application, in particular for analytical applications.

The achievement of this objective by the present invention is delineated in the characterizing part of Claim 1.

Further means for achieving the objective or embodiments of the present invention are delineated in Claims 2 through 23.

By using additive nanolithography to produce such miniaturized terahertz radiation sources, one is able to produce field electron sources having a high directional beam value. By employing additional miniaturized, electron-optical elements,

such as accelerator grids, focusing lenses, beam deflectors, and free-standing metallic rods, the components may now be assembled to construct a miniaturized, free electron laser on a surface of a few $100 \mu\text{m}^2$ through 10 mm^2 . In this context, the 5 electron source has the characteristic of emitting electrons at 30 volts, which then possess an energy of 30 electron volts. Using nanolithography, it is possible to control the second characteristic component of focusing and beam guidance of the electron beam in parallel to the surface at a finite 10 distance to the third component, a metallic grating. The vertical position of the beam over the metallic grating may likewise be adjusted by applying deflection voltages to 15 micro-miniaturized deflecting plates or wire lenses. The diffraction grating, to the extent that is possible, up to one millimeter long, a reflection diffraction grating having a 20 grating constant in the range of 0.1 mm to $0.1 \mu\text{m}$, may be produced using conventional lithography in the manufacturing of electrical connection structures for supplying the field electron source, i.e., be defined by electron-beam lithography 25 at the highest resolutions.

A high-resolution double-resist technique and lift-off are advantageously used. The present approach employs new types of 25 technologies to integrate the electron source, the beam guidance, and the generation of the far-infrared radiation by the flight of the fast electrons across the diffraction grating. In this context, given standard sources of up to approximately 20,000 volts accelerating voltage and an 30 electron beam of $20 \mu\text{m}$ diameter over a grating of 100 to 300 μm period, an infrared radiation in the far infrared is achieved between $100 \mu\text{m}$ and one millimeter wavelength. This 35 radiation is produced by the image charge which oscillates in response to the electrons flying past the surface profile of the grating. The changing spacing between the charges produces an oscillating dipole, which oscillates in coherent fashion along the grating. This ensues due to the Coulomb interaction of the individual charges on the wires. In this context, the

entire electrical field oscillates coherently in conformance with the individual charges of the rods. In this manner, electromagnetic radiation is emitted coherently along the entire grating. Its energy transfer from the electron beam to
5 the electromagnetic radiation takes place virtually losslessly. The polarization requires a certain displacement current and, thus, a certain power, but this is entirely drawn directly from the beam. The oscillating dipole charge chain is produced in this manner. Also novel is integration of the
10 electron guidance on a chip, and the direct coupling to the grating having a high spatial resolution, in the manufacturing process. Just as novel is that micro-miniaturization is making possible the use of low-energy electrons having energies of between 10 and 1000 eV. It is also possible to generate up to
15 10 kV of electrons on the chip and to implement the guidance by using miniaturized electron-optical components, such as micro-lenses and deflecting elements.

When using such high-energy electrons, radiation may also be
20 generated for short wavelengths ranging from middle infrared to the visible spectral region. By manufacturing on a common substrate, one ensures direct coupling to the grating via the shortest distance to the source, and the manufacturing of the grating and the source on the same chip. In this manner, the
25 path of rays of the electrode configuration, which in the conventional design, is up to one meter, is reduced to less than 1 mm to 10 mm length. Moreover, a very highly coherent and local light source is produced, which benefits the temporal and spatial coherence of the radiation. Because the
30 entire electron path is shortened to a greater degree, it is no longer necessary to use extra-high or high vacuum in the radiation room. It suffices to cover the system by a window etched in silicon using a flipchip bonding technique. This window is closed by a continuous membrane of silicon, thereby
35 rendering possible a hollow space. The up to 10 μm high component is easily accommodated in the hollow space.
Typically, into a silicon wafer of 250 μm thickness, one

etches windows of a few millimeter diameter, which are sealed by a membrane having a thickness of 10 μm up to 100 μm . This renders possible a stable mechanical encapsulation of the miniaturized component. However, it can also be manufactured 5 micromechanically, in millimeter dimensions. In this context, the required vacuum is approximately 0.01 Torr. In this case, the average free path length of the electrons in this gas of reduced pressure is as large as the beam length of the miniaturized component. This eliminates the need for a pump 10 configuration, which is a significant advantage. The component can be packaged as a ready-made, sealed element and connected. In this manner, it is possible to produce a terahertz 15 radiation source, i.e., a millimeter and submillimeter radiation source on a semiconductor chip. Through appropriate wave guidance, this radiation source can be linked to further 20 applications.

Further advantages, features, and possible applications of the miniaturized or micro-miniaturized terahertz radiation source, in particular its design and mode of operation, may be derived 25 from the following description in conjunction with the exemplary embodiments depicted in the drawing.

The present invention shall now be elucidated on the basis of 30 exemplary embodiments depicted in the drawing. The terms and assigned reference symbols employed in the appended reference symbol list are used in the Specification, the Claims, the Abstract, and in the drawing.

35 In the drawing:

Figure 1 shows a plan and side view of a fundamental design of a miniaturized terahertz radiation source based on the Smith Purcell effect;

Figure 2 illustrates an encapsulation having a silicon membrane structure for maintaining the

necessary vacuum during operation; and

Figure 3 depicts a two-chamber membrane covering of the miniaturized, free electron laser.

Figure 1 schematically depicts the electrode design for a miniaturized, free electron laser in a plan view and side view. The individually illustrated elements are also produced using a known additive nanolithography method. Shown both in the plan view as well as in the side view, the individual elements of the miniaturized terahertz radiation source are illustrated in the following sequence. First, field emitter tips 1 are shown to the left. They are linked via electrical terminals or connections 2 to a controllable voltage source 3 and, on the other hand, to an electrostatic lens 4, composed here of three electrodes. The left electrode is the extractor or the first anode of the electron source. Shown in the middle are beam deflectors 5 having connections 6, to which optical and/or electron-beam lithography and a deflection voltage are applied. Beam deflector 5 is followed by a grating 7 of metal. Electron beam 9, having been deflected by beam deflector 5, passes through this grating and strikes here as an electron beam, without being deflected 10, upon a second anode 8.

Figure 2 shows one variant of an encapsulation. This design enables the electron source, here in the form of field emitter tips 1, electrostatic lens 4 for focusing electron beam 9/10, beam deflector 5 for deflecting the beam in the horizontal and vertical direction, grating 7 of metal having an underlaid reflector to be constructed in integrated fashion, using mix-match technology employing additive nanolithography on an insulating substrate having a terahertz reflection base in the grating region, on metal conductor connection structures, which are prefabricated using electron beam or optical lithography, and to be imperviously encapsulated in a vacuum 13 using a technology which is transparent to terahertz radiation. This design enables electron beam 9 emerging from

field emitter 1 to be focused through miniaturized wire lenses 4, to be directed through integrated deflecting plates 5 relatively to the position of grating 7, and to be positioned, thereby generating terahertz radiation, whose intensity and 5 wavelength may be varied and selected. Field emitters, i.e., field emitter tips 1 are linked via an electrical terminal connection 2 to a controllable voltage source 3 and, moreover, via an electrical connection 2 to the middle electrode of electrostatic lens 4. The left electrical electrode of lens 4 10 is the first anode of the electron source and, together with a terminal of controllable voltage source 3, is connected to ground, as is also the electrode of electrostatic lens 4 situated on the other side of the middle electrode. The field 15 electron source having field emitters 1 is a wire constructed, using additive nanolithography, out of readily conductive material having stabilizing series resistance, and is designed such that electron beam 9 emerges in parallel to the surface. This means that the wire is manufactured, using a 20 computer-controlled deposition lithography, in a straight or curved design, to end freely over the surface of the conductor path structure. The field electron source has a punctiform design. On its field emitter tips (1), a material having a low work function is deposited using additive nanolithography, so 25 that electrons are emitted already in response to relatively low voltages.

One variant of the design provides for mounting an accelerator grid as a beam deflector 5, in the form of a free-standing electrode composed of two cylindrical rods or a standing wire 30 ring, behind the field electron source having field emitters 1. The intention here is for the electrons to be accelerated and directed into subsequent, additionally constructed round multipole lenses and/or cylindrical lenses, so that the 35 propagating electron beam 9 is additionally deflected over subsequent diffraction grating 7 at a homogeneous distance to the surface. The focusing and beam-guidance lenses, which are implemented by additive nanolithography on the metal

connection structure produced using electron-beam lithography or optical lithography, are constructed, using this technology, to produce a diffraction grating having a length of approximately 1 mm to 1 cm, with grating periods of 0.5 to 5 10 μm , depending on the wavelength of the terahertz radiation to be emitted.

One variant of the design also provides for a side-by-side configuration of a plurality of electrically isolated 10 diffraction gratings, which may be activated by selecting various sources, enabling various emitted wavelengths to be chosen.

15 The radiation from electron source is retained at a constant level by a control circuit, in particular by a controllable voltage source 3, and electron beam 10 propagating over grating 7 is then picked up by a second anode 8, which is used as a collecting anode electrode.

20 Between the second earth electrode of electrostatic lens 4 and second anode 8, a field is applied, which may be used to alter the electron velocity along the grating. This is used for precisely adjusting the wavelength and also for generating a frequency spectrum.

25 Another exemplary embodiment of the design of the miniaturized, i.e., microminiaturized terahertz radiation source, based on the Smith-Purcell effect, is shown in Figure 2. By providing encapsulation using a silicon membrane 30 structure, the required vacuum 13 may be maintained for operating the laser. The emitted laser THz radiation 15 is radiated to the outside through a membrane window 14. The radiation emitter, constructed on a chip of silicon 11 and composed of the field emission source, optics, grating and 35 anode, is covered in this exemplary embodiment by membrane window 14, which is made of silicon 11, as is the entire covering chip 16. The thus constructed radiation emitter is

evacuated in a vacuum system, prior to the bonding, to a pressure of 10^{-4} , which suffices for one millimeter average free path length. The hollow space is subsequently sealed in the vacuum by thermal bonding, without short-circuiting the
5 voltage supply. Membrane windows 14 in covering chip 17 are treated using reflection-reducing layers, so that a maximum transmission through window 14 is attained for the frequency range of the emitted radiation.

10 Configured underneath the grating region is a THz radiation reflector in the form of a metal layer or arrangement of grating rods, having a defined spacing of a suitable period, of magnetic or non-magnetic materials, so THz radiation 15, which exits grating 7 in the direction of the substrate, is
15 sent back through the grating with the highest possible reflectance, thereby strengthening the intensity of the emitted radiation. Implementing a beam guidance over grating 7 at a defined distance makes it possible to vary the intensity of the radiation source. This means that by employing
20 deflecting element 5 before the grating, the radiated intensity may be modulated in response to the application of an a.c. voltage to this deflecting element. In this manner, the radiation may be directly generated in modulated form for spectroscopic purposes for lock-in measuring techniques. The
25 same lock-in modulation may also be provided by modulating the extraction voltage at field emitter tip 1.

30 For certain applications, it is beneficial to supplement the voltage source by installing a monochromator on an overlying surface. Such a monochromator is constituted as a nanometer structure or micrometer structure that acts on this region, so that beams generated with a different wavelength exit the radiation source in different directions. In this manner, by switching over the electron energy, which, in the
35 electrostatic system in accordance with the electrostatic principle, always yields the same focusing and, thus, constant operating conditions, radiation of different frequencies may

be generated, and the radiation source may be electrically tuned for different applications.

Between focusing lens 4 and the end of grating 7, one variant 5 provides for applying an electrical field, in which, at the end of the grating, an additional electrode is positioned, through which voltage may be applied to accelerate or decelerate the flying electrons. This makes it possible to 10 compensate for the energy loss experienced by the electrons when flying past grating 7. Grating 7, over which electron beam 10 propagates, is subdivided into regions which are disposed in parallel to the beam direction, in which different 15 grating constants are implemented. The horizontal, electrostatic beam guidance, effected by electrodes positioned in parallel to grating 7 and, respectively, by a plurality of electron sources, one of which is assigned to the individual region, now makes it possible for the emitted radiation to be implemented as radiation that is switchable in its wavelength.

20 The grating constant of the grating varies transversely to the beam direction, so that the beam guidance may be varied over the grating by deflection fields or by deflecting plates, which surround the grating all around, and are positioned behind the focusing lens, such that a region having a 25 different grating constant may be selected for emitting the wavelength of the radiation. Designing the grating as a "chirped grating", i.e., as a grating having a variable grating constant, enables the wavelength to be adjusted in continuous fashion.

30 The intensity of the terahertz radiation source is controlled by installing an electrostatic plate, which is transparent to THz radiation, below and above the grating, thereby enabling the intensity to be locally selected. This is advantageously 35 achieved by designing these electrostatic plates to include regions of different potentials, i.e., by providing separately adjustable strips.

Figure 3 shows another exemplary embodiment, where two membrane windows 14 are provided in covering chip 17. As in Figure 2, it can also be discerned here quite clearly that covering chip 17 is insulated from the electrodes and the 5 electrode connections by an insulator of silicon 16. At the same time, this is also constituted of bond region 7 for providing hermetic sealing when encapsulating the arrangement. The construction includes, in turn, the substrate of silicon 11 having a silicon dioxide layer 12. Positioned thereon are 10 field emitter 1, lenses 4, grating 7 and second anode 8. Here, again, the first anode is the left electrode of electrostatic lens 4. Also positioned, in turn, is grating 7 of metal, out of which the emitted terahertz radiation 15 emerges. Electron beam 10 impinges, without deflection, on second anode 8 having 15 electrical connection 2. The one membrane window 14 is provided with a lens 19 for focusing THz radiation 15. Due to the specially formed covering chip 17, a vacuum 13 is provided in both chambers 18, 18'; a getter pump (not shown), including its material, may be set in operation in second chamber 18' by 20 a one-time activation in response to current flow, to bring the entire volume of both chambers to the required operating pressure.

In a further variant (not shown), ionic getter materials, 25 capable of being activated by the electrical connection, are applied to the chip, next to the Smith-Purcell element. These materials are used for pumping out the bonded and encapsulated structure. Such a manufacturing, employing additive nanolithography on metal conductor-connection structures, 30 which are prefabricated by electron beam lithography or optical lithography, include integrated grating structures on an insulating substrate, in particular silicon oxide, and a THz underlaid reflector integrated in the grating region, renders possible a component which may be used and set up in 35 any position as a THz radiation source in modular form.

Reference Symbol List

- 1 field emitter (tips)
- 2 electrical terminal or connections
- 5 3 controllable voltage source
- 4 electrostatic lens
- 5 beam deflector or deflecting plates
- 6 electrical connections for beam deflectors
- 7 metal grating
- 10 8 second anode
- 9 electron beam
- 10 electron beam without deflection
- 11 silicon (Si)
- 12 silicon dioxide (SiO₂)
- 13 vacuum
- 14 membrane window of silicon
- 15 emitted terahertz radiation
- 16 insulator or bond region for vacuum-tight
encapsulation of the arrangement
- 20 17 covering chip
- 18, 18' chambers
- 19 lens for focusing the THz radiation

What is claimed is:

1. A miniaturized terahertz radiation source based on the Smith-Purcell effect, in which, from a focused electron source, a high-energy bundle of electrons is transmitted at a defined distance over a reflection diffraction grating composed of transversely disposed grating rods, so that, in response to an image charge oscillating within the profile of the grating, an electromagnetic wave of one wavelength is emitted, which is adjustable as a function of the periodicity of the lines and of the electron velocity,

wherein the elements of the radiation source, such as field emitter (1), electrostatic lens (4), beam deflector (5), grating (7) of metal, and a second anode (8), are integrated on a semiconductor chip using additive or known nanolithographic methods.

2. The miniaturized terahertz radiation source as recited in Claim 1,

wherein the field electron source is conceived as a wire constructed using additive nanolithography, out of readily conductive material having stabilizing series resistance; and

the wire is positioned, using computer-controlled deposition lithography, in a straight or also curved design, to end freely over the surface of the conductor path structure for the electrical terminals and connections (2) in field emitter tips (1).

3. The miniaturized terahertz radiation source as recited in
Claims 1 and 2,

wherein the field electron source has a punctiform design, and a material, which has a low work function and emits electrons already in response to relatively low voltages, is deposited on its field emitter tip(s) (1), using additive nanolithography.

4. The miniaturized terahertz radiation source as recited in
Claims 1 through 3,

wherein the elements are encapsulated in a vacuum-tight manner by a covering chip (17).

5. The miniaturized terahertz radiation source as recited in
Claims 1 through 4,

wherein the beam deflector (5) for deflecting the electron beam (9) in the horizontal and vertical direction, as well as the grating of metal (7) having an underlaid reflector are constructed in integrated fashion, using mix-match technology, employing additive nanolithography or also employing electron beam or optical lithography, on prefabricated metal conductor connection structures having integrated grating structures, on a layer of silicon dioxide (12) of a substrate of silicon (11), having a THz reflector base in the grating region, and the entire arrangement is imperviously encapsulated so as to be transparent to terahertz radiation (15);

the electron beam (9) emerging from the integrated electron source is focused through the electrostatic lens (4), in the form of miniaturized wire lenses, and is able to be guided and positioned by integrated deflecting

plates (5) in relation to the position of the reflection diffraction grating (7); and

a terahertz radiation (15) is thereby produced whose intensity and wavelength is able to be varied and selected.

6. The miniaturized terahertz radiation source, in particular as recited in the first part of Claim 1,

wherein to accelerate the electrons behind the field electron source, an accelerator grid, in the form of a free-standing electrode composed of two cylindrical rods or a standing wire ring, is positioned behind the field electron source; and

the accelerated electrons arrive in round multipole lenses or cylindrical lenses of an electrostatic lens (4) configured subsequent to the accelerator grid, and an electron beam propagates, without being deflected (10), over a subsequent reflection diffraction grating (7) at a homogeneous distance to the surface.

7. The miniaturized terahertz radiation source as recited in one of Claims 1 through 6,

wherein a reflection diffraction grating (7), fabricated using this technology, having a length of approximately 1 mm to 1 cm, and grating periods of between 0.5 to 10 μm , depending on the wavelength of the terahertz radiation (15) to be emitted, is positioned subsequent to the electrostatic lens (4) and the beam deflector (5), which are implemented using additive nanolithography on the metal structure produced using electron-beam lithography or optical lithography.

8. The miniaturized terahertz radiation source as recited in

one of Claims 1 through 7,

wherein a plurality of electrically isolated diffraction gratings are positioned side-by-side as gratings of metal (7), which are able to be activated in response to the selection of various sources for selecting different emitted wavelengths.

9. The miniaturized terahertz radiation source as recited in one of Claims 1 through 8,

wherein ionic getter materials, capable of being activated by an electrode, are applied to a semiconductor chip, next to the Smith-Purcell element, to produce and maintain the required vacuum (13) in the bonded and encapsulated structure.

10. The miniaturized terahertz radiation source as recited in one of Claims 1 through 9,

wherein to stabilize the radiation from the electron source, a controllable voltage source (3) is connected via electrical terminals or connections (2) to the electron source; and

the beam (9) exiting the field emitter tips (1) is collected on an electrode of the arrangement being used as a second anode.

11. The miniaturized terahertz radiation source as recited in one of Claims 1 through 10,

wherein to precisely adjust the wavelength and/or generate a desired frequency spectrum, a voltage is applied between the earth electrode of the electrostatic lens (4) and the electrode acting as a second anode, to alter the electron velocity along the grating (7).

12. The miniaturized terahertz radiation source, in particular as recited in one of Claims 1 through 11,

wherein the miniaturized terahertz radiation source, which is constructed on a semiconductor chip, and includes field emitters, i.e., field emitter tips (1), optics of an electrostatic lens (4), a grating (7), and a second anode (8), is covered by a membrane window (14) etched using a silicon membrane technique, and is able to be evacuated in a vacuum system prior to the bonding operation to a pressure within a range of 10^{-4} Torr, which suffices for an average free path length of one millimeter; and

the chamber(s) (18, 18') is (are) constructed in the vacuum system, using thermal bonding, so as to be able to be encapsulated and/or sealed, without short-circuiting the voltage supply.

13. The miniaturized terahertz radiation source as recited in one of Claims 1 through 12,

wherein two membrane windows (14) are positioned next to one another in the covering chip (17), for two chambers (18, 18'); and

in one of the two membrane windows (14), a getter pump is

set in operation by a one-time activation in response to current flow, and the entire volume of both formed chambers (18, 18') receives the required operating pressure.

14. The miniaturized terahertz radiation source as recited in one of Claims 1 through 13,

wherein the membrane windows (14) in the covering chip (17) are treated with additionally applied layers to reduce reflection.

15. The miniaturized terahertz radiation source as recited in one of Claims 1 through 14,

wherein configured underneath the grating region is a terahertz radiation reflector in the form of a metal layer or in the form of an arrangement of grating rods, having a defined spacing of a suitable period, of magnetic or non-magnetic materials for strengthening the intensity of the emitted terahertz radiation (15).

16. The miniaturized terahertz radiation source as recited in one of Claims 1 through 15,

wherein the intensity of the radiation source is variable in response to the beam guidance over the grating of metal (7) at a defined distance; the radiated intensity is able to be modulated in response to the application of an a.c. voltage to this deflecting element, by employing an additional deflecting element before the grating (7).

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17. The miniaturized terahertz radiation source as recited in one of Claims 1 through 15,

wherein the terahertz radiation (15) is able to be generated as modulated radiation for spectroscopic purposes; and

the same lock-in modulation is also able to be generated by modulating the extraction voltage at field emitter tip (1).

18. The miniaturized terahertz radiation source as recited in one of Claims 1 through 17,

wherein the source is supplemented by installing a monochromator on an overlying surface, in the form of a nanometer structure or micrometer structure that acts on this region; and

terahertz radiation (15), which can be generated with a different wavelength, exits the source in different directions.

19. The miniaturized terahertz radiation source as recited in one of Claims 1 through 18,

wherein an electrical field is applied between the electrostatic lens (4) for focusing, and the end of the grating (7), in that an additional electrode of the second anode is positioned at the end of the grating which, through the applied voltage, either accelerates or decelerates the flying electrons.

20. The miniaturized terahertz radiation source as recited in one of Claims 1 through 19,
wherein the grating (7) is subdivided into regions which are disposed in parallel to the beam direction and in which different grating constants are implemented; and a lateral deflecting element for beam guidance and/or wavelength selection is mounted around the grating regions, and/or groups of field emitters are selectively driven.

21. The miniaturized terahertz radiation source as recited in one of Claims 1 through 20,
wherein the grating (7) varies in its grating constant transversely to the beam direction, so that deflection fields or deflecting plates, which surround the grating (7) all around, are positioned as beam deflectors (5), such that the beam guidance over the grating (7) is variable in such a way that one region having a different grating constant is selected for emitting the wavelength of the terahertz radiation (15), and, in particular, in the case of a grating (7) having a variable grating constant, the wavelength is continuously adjustable.

22. The miniaturized terahertz radiation source as recited in one of Claims 1 through 21,
wherein an electrostatic plate, which is transparent to the terahertz radiation (15), is positioned to provide intensity control below and above the grating (7), and enables the position of the electron beam (10) to be varied in the entire grating region.

23. The miniaturized terahertz radiation source as recited in one of Claims 1 through 22.

wherein the radiation source is designed as a component that is available in modular form and is usable in any spatial situation.

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Abstract

A miniaturized terahertz radiation source based on the Smith-Purcell effect is provided, in which, from a focused 5 electron source, a high-energy bundle of electrons is transmitted at a defined distance over a reflection diffraction grating composed of transversely disposed grating rods, so that, in response to oscillating image charges, electromagnetic waves of one wavelength are emitted, the wavelength being adjustable as a function of the periodicity 10 of the lines and of the electron velocity. The elements of the radiation source, such as field emitter (1), electrostatic lens (4), beam deflector (5), grating (7) of metal, and a second anode (8), are integrated on a semiconductor chip using 15 additive nanolithographic methods. The field electron source is constructed to project, as a wire, out of the surface, using additive nanolithography, and is made of readily conductive material having stabilizing series resistance. The wire is constructed, using computer-controlled deposition 20 lithography, in a straight or curved, free-standing design. In its surface area, the base material bears a conductor structure for the electrical terminals and connections (2), including controllable voltage sources (3) for supplying the field emitter tips (1), lens (4), and control electrodes (5, 25 8). The terahertz radiation source is designed to be a powerful component that is available in modular form and is usable in any spatial situation.

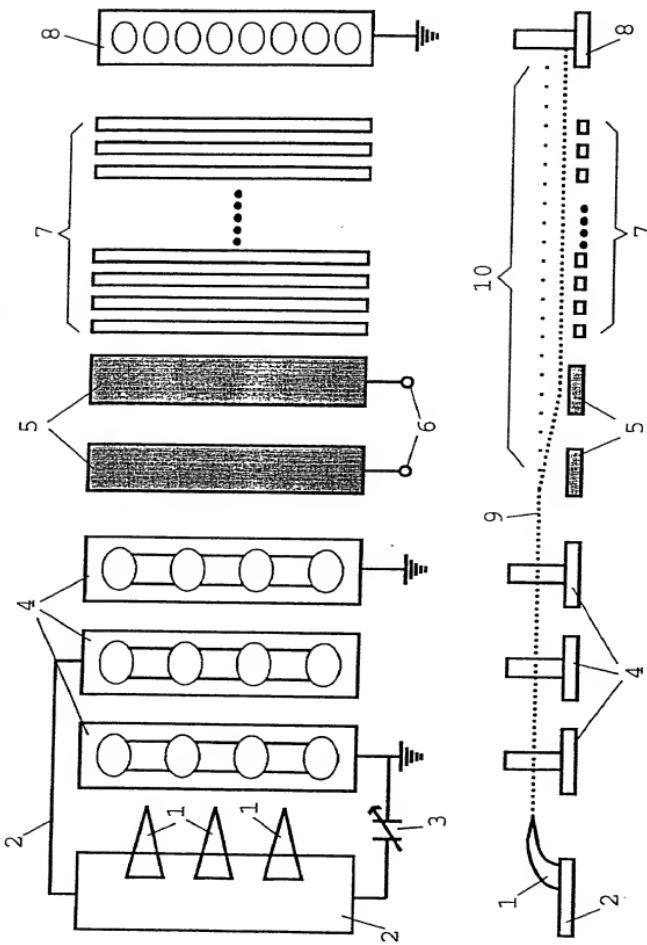


FIG. 1

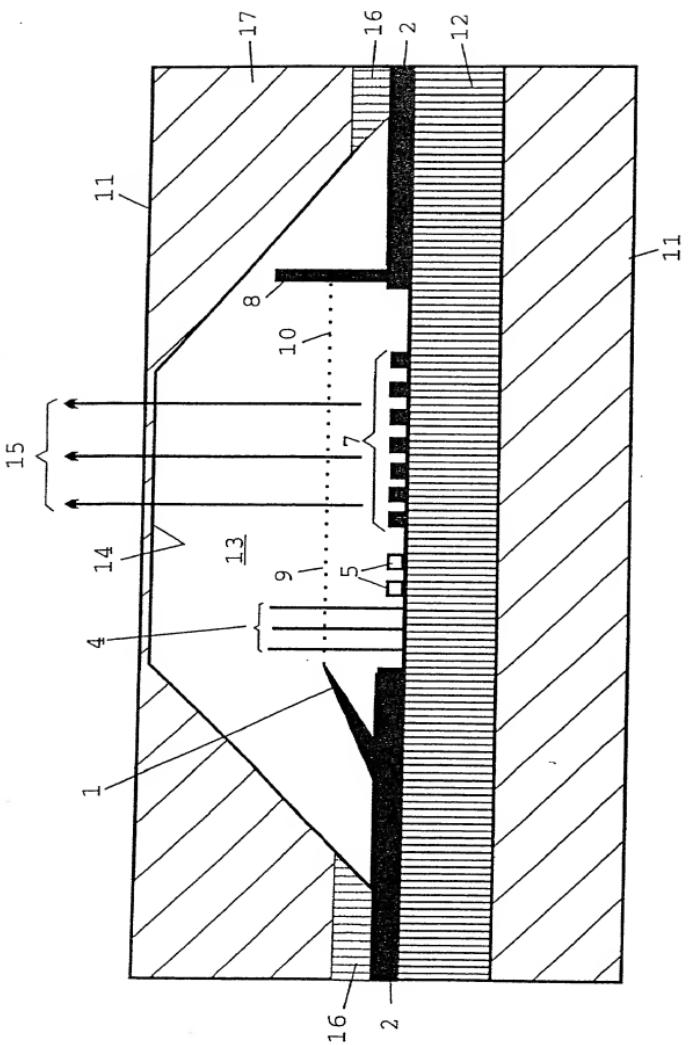


FIG. 2

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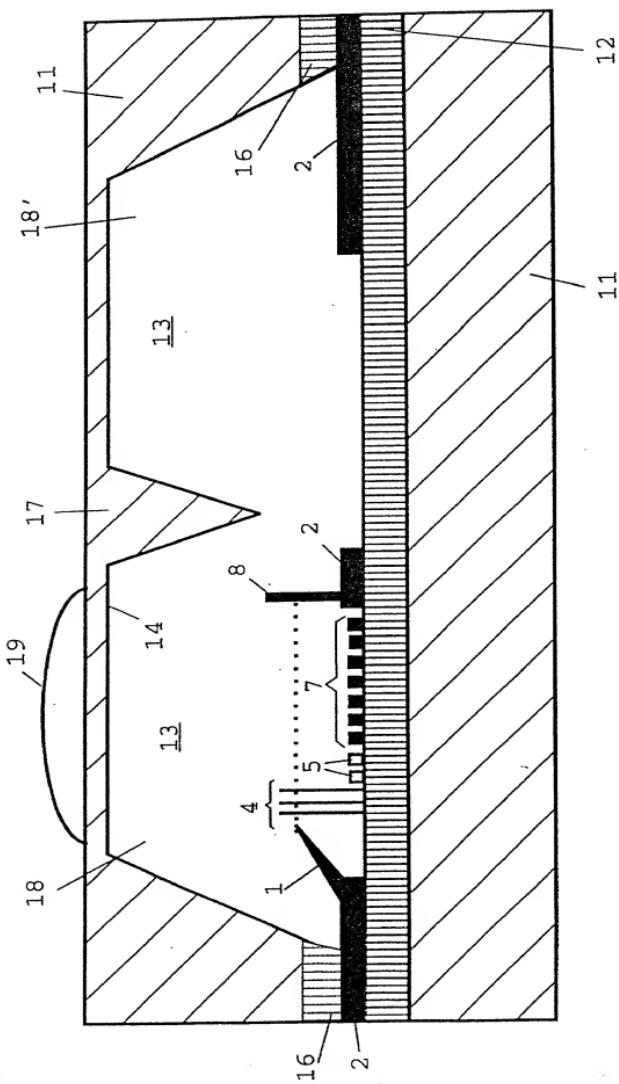


FIG. 3

DECLARATION AND POWER OF ATTORNEY

As a below named inventor, I hereby declare that:

My residence, post office address and citizenship are as stated below next to my name.

I believe I am the original, first and sole inventor (if only one name is listed below) or an original, first and joint inventor (if plural names are listed below) of the subject matter which is claimed and for which a patent is sought on the invention entitled **MINIATURIZED TERAHERTZ RADIATION SOURCE** the specification of which was filed as International Application No. PCT/EP00/04167 on May 10, 2000 and filed as U.S. application on November 26, 2001 having U.S. Serial No. 09/980,250 for Letters Patent in the U.S.P.T.O.

I hereby state that I have reviewed and understand the contents of the above-identified specification, including the claims.

I acknowledge the duty to disclose information which is material to the examination of this application in accordance with Title 37, Code of Federal Regulations, § 1.56(a).

I hereby claim foreign priority benefits under Title 35, United States Code, § 119 of any foreign application(s) for patent or inventor's certificate listed below and have also identified below any foreign application(s) for patent or inventor's certificate having a filing date before that of the application on which priority is claimed:

PRIOR FOREIGN APPLICATION(S)

Number	Country Filed	Day/Month/Year	Priority Claimed Under 35 USC 119
199 23 614.3	Fed. Rep. of Germany	May 25, 1999	Yes

And I hereby appoint Richard L. Mayer (Reg. No. 22,490), Gerard A. Messina (Reg. No. 35,952) and Linda M. Shudy (Reg. No. 47,084) my attorneys with full power of substitution and revocation, to prosecute this application and to transact all business in the Patent and Trademark Office connected therewith.

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I hereby declare that all statements made herein of my own knowledge are true and that all statements made on information and belief are believed to be true; and further that these statements were made with the knowledge that willful false statements and the like so made are punishable by fine or imprisonment, or both, under Section 1001 of Title 18 of the United States Code and that such willful and false statements may jeopardize the validity of the application or any patent issued thereon.

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